

Magnetic design of small-aperture dipoles of the shell and block type

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- Choice of design parameters
- Shell vs. Block type design:
 - conductor efficiency
 - field quality
- Two-in-one: yoke diameter requirement
for horizontal vs. vertical layout
- Conclusions

Aperture requirement

SSC: $40 \rightarrow 50$ mm LHC: $50 \rightarrow 56$ mm

VLHC: $50 \rightarrow 30$ mm?

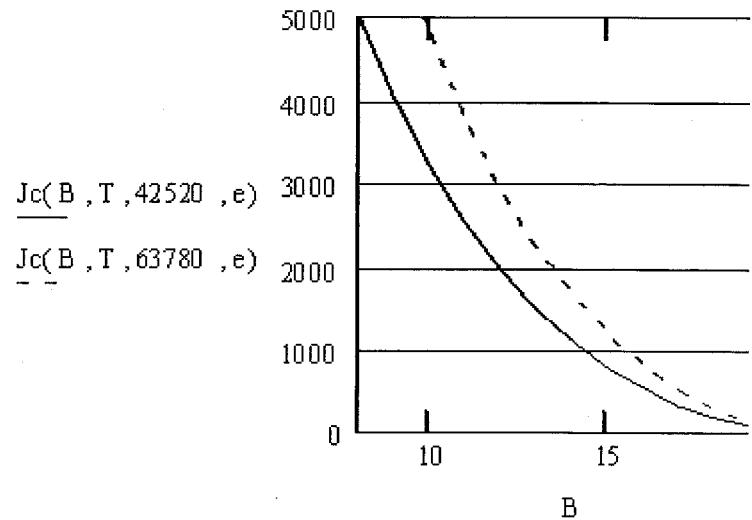
Charge: Guided by the snowmass '96 parameter set, explore and develop innovative concepts that will result in significant cost reductions.

Critical current density

$$J_c(B, T, C_0, e) = \frac{C(C_0, e)}{B} \cdot \frac{B}{B_{c2}(T, e)}^2 \cdot \frac{T}{T_{c0}(e)}^2$$

(Summers, L, IEEE Trans. M

$$J_c(12T, 4.2K) = 2 - 3 \text{ kA}$$



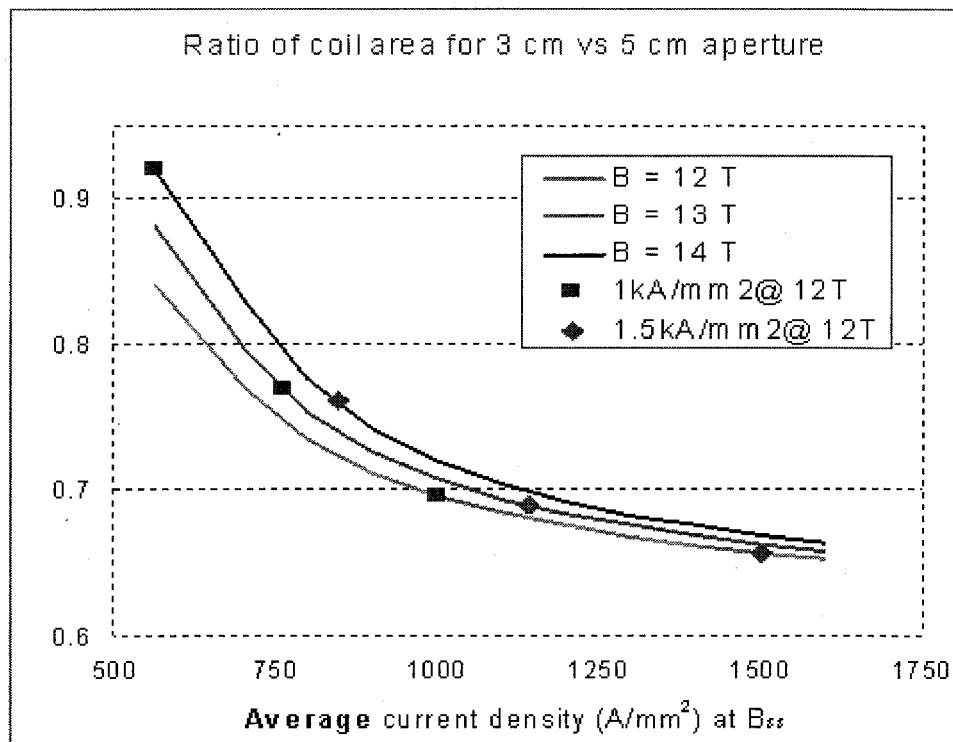
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Choice of design parameters: conductor efficiency



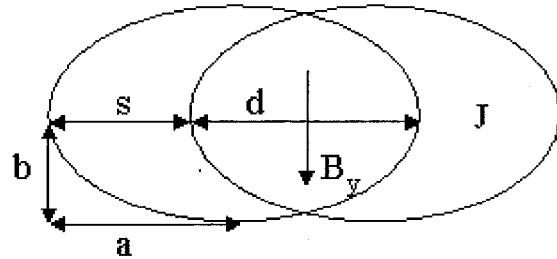
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Based on intersecting ellipses model



$$By = -\frac{\mu_0 J sb}{a+b}$$

$$\frac{s(J, d, B)}{B} = \frac{2 \cdot d \cdot B}{\mu_0 \cdot J \cdot d}$$

$$a(J, d, B) = \frac{s(J, d, B)}{2}$$

$$\frac{d}{2}$$

$$b(J, d, B)$$

$$A_{eq}(J, d, B) = a(J, d, B) \cdot b(J, d, B) = \frac{\pi}{4} \cdot \frac{1}{2} \cdot \frac{s(J, d, B)}{a(J, d, B)} \cdot \frac{1}{2} \cdot \frac{s(J, d, B)^2}{4 a(J, d, B)^2} = \frac{1}{2} \cdot \frac{s(J, d, B)^2}{2} \cdot \frac{1}{2} \cdot \frac{\sin}{2}$$

$$A_{hc}(J, d, B) = \frac{\pi \cdot a(J, d, B) \cdot b(J, d, B)}{2} = A_{ap}(J, d, B)$$

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Design parameters

Coil aperture	:	30 mm
Coil width	:	27 mm
Coil layout	:	shell/block
No. of layers	:	3
Maximum field	:	12 T ($J_c(12T, 4.2K)=2\text{ kA}/i$) 13 T ($J_c(12T, 4.2K)=3\text{ kA}/i$)
Geom. Harmonics	:	$< 10^{-4}$ @ 1cm
Stress (Lorentz)	:	$< 100\text{ MPa}$

Shell type design: cable parameters

Strand diameter	mm	0.75
Cu/Sc ratio		1:1
No. of strands		24
Area of superconductor	mm ²	5.301
Cable width (bare)	mm	9.0
Cable mid-thickness (bare)	mm	1.35
Keystone angle	deg	1.8
Transposition length	mm	120
Compaction (area)	%	88.3
Compaction (inner edge)	%	80
Compaction (outer edge)	%	100
Radial insulation	mm	0.150
Azimuthal insulation	mm	0.120

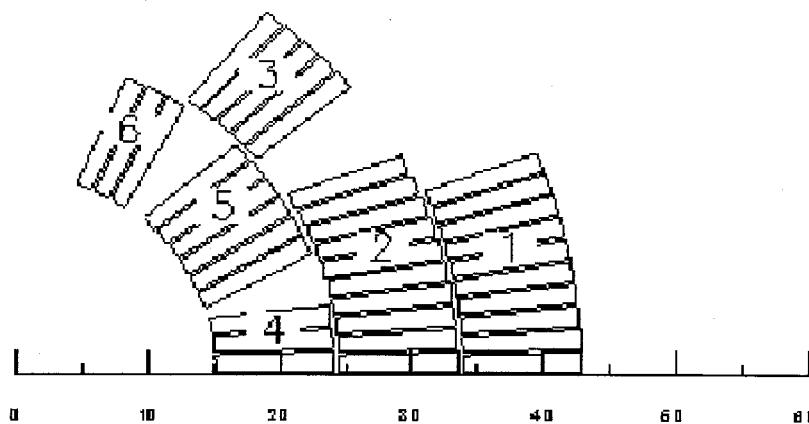
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Shell-type design: coil cross-section



- 3 layer, 6 block design

- Optimized with F

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Shell-type design: coil cross-section

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- 3 layer, 6 block design

- Optimized with F

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Block type design: cable parameters

Strand diameter	mm	0.75
Cu/Sc ratio		1:1
No. of strands		24
Area of superconductor	mm ²	5.301
Cable width (bare)	mm	9.0
Cable mid-thickness (bare)	mm	1.35
Keystone angle	deg	0.0
Transposition length	mm	120
Compaction (area)	%	88.3
Compaction (inner edge)	%	90
Compaction (outer edge)	%	90
Radial insulation	mm	0.150
Azimuthal insulation	mm	0.120

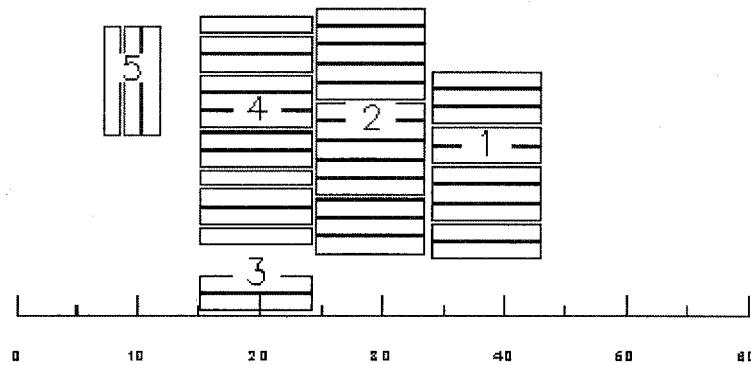
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Block-type design: coil cross-section



- 3 layer, 6 block design

- Optimized with R

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Block-type design: coil cross-section

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- 3 layer, 6 block design

- Optimized with R

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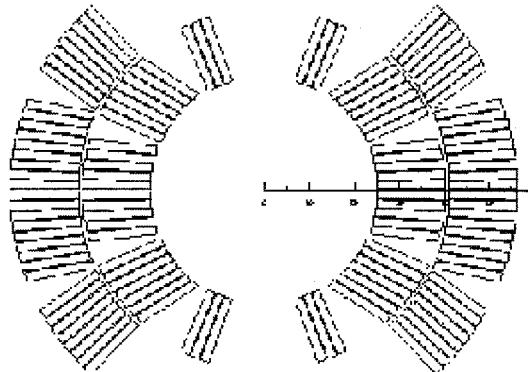
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50 mm bore, 2 layer shell type dipole design

- FNAL/LBL/KEK collaboration
- Cross section from FNAL TD-98-035
- Optimization work still underway (last update Oc



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50 mm bore dipole, 2 layer, shell type design

- FNAL/LBL/KEK collaboration
- Cross section from FNAL TD-98-035
- Optimization work still underway (last update Oct 1998)

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Short sample performance/conductor efficiency

Parameter	Unit	Shell	Block	50 mn
SC area (1 quadrant)	mm ²	196	212	398
$J_c(12T, 4.2K) = 2 \text{ kA/mm}^2$				
I_{ss}	kA	10.1	10.1	18.0
$B_{ss}^{(0)}$	T	11.9	12.0	12.9
$B^{(\max)}$ (layer 1)	T	12.2	12.2	13.2
$B^{(\max)}$ (layer 3)	T	6.2	5.3	
$J_c(12T, 4.2K) = 3 \text{ kA/mm}^2$				
I_{ss}	kA	11.0	11.1	19.4
$B_{ss}^{(0)}$	T	13.0	13.1	13.9
$B^{(\max)}$ (layer 1)	T	13.3	13.3	14.2
$B^{(\max)}$ (layer 3)	T	6.8	5.8	

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Energy and forces

Parameter	Unit	Shell	Block	50
Operating current	kA	10.2	10.1	10
Stored energy	MJ/m	0.35	0.41	0.4
Inductance	mH/m	6.7	8.0	5.5
$-\Sigma F_y$ (1 quadrant)	MN/m	0.9	0.8	1.1
ΣF_x (1 quadrant)	MN/m	2.0	2.3	3.3
Stress (Φ/y , 1 st layer)	MPa	86	28	110
Stress (Φ/y , 2 nd layer)	MPa	84	36	77

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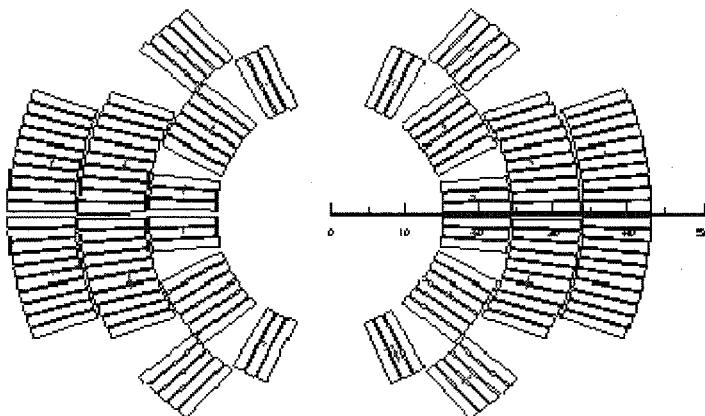
Geometric harmonics

10^{-4} @ 1cm

Component	Shell	Block	50 mm
b_3	0.1	-0.1	0.0
b_5	0.3	0.3	-0.1
b_7	0.7	0.6	0.0
b_9	0.6	-0.8	0.1
b_{11}	2.9	1.2	0.0
b_{13}	-0.5	0.2	0.0

Random errors

Random block displacement simulation using ROXIE
Shell: +/- 50 μm radial/azimuthal displacements
Block: +/- 50 μm horizontal/vertical displacements



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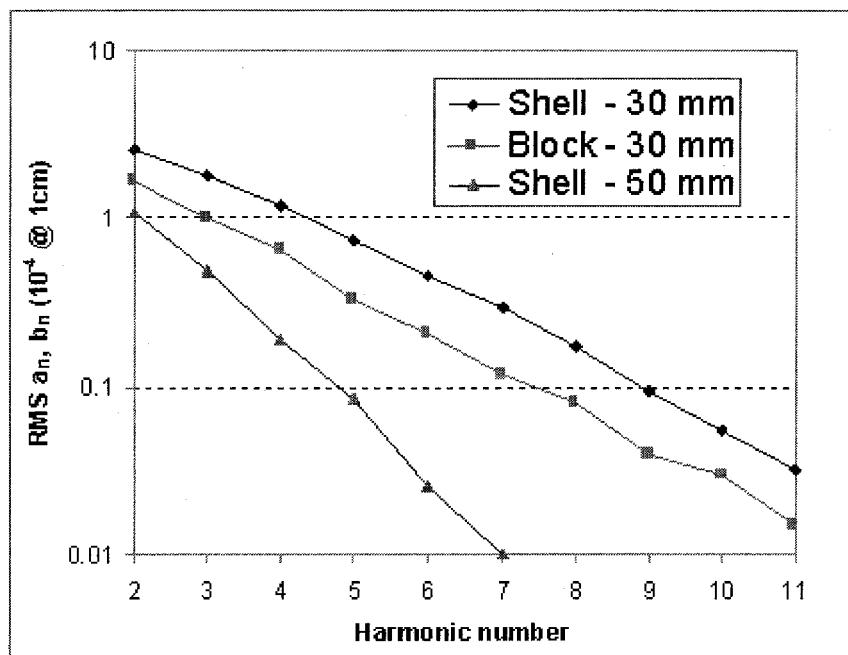
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Random errors

Random block displacement simulation using ROXIE
Shell: +/- 50 μm radial/azimuthal displacements
Block: +/- 50 μm horizontal/vertical displacements

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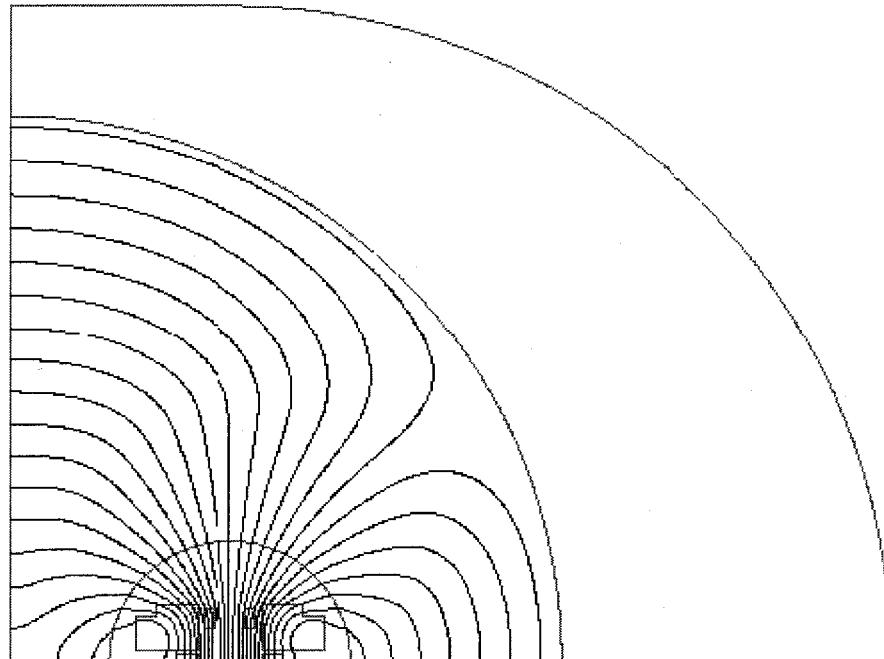
Random errors



- No longitudinal averaging

- Magnetic measurement

Horizontal two-in-one layout



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Horizontal two-in-one layout

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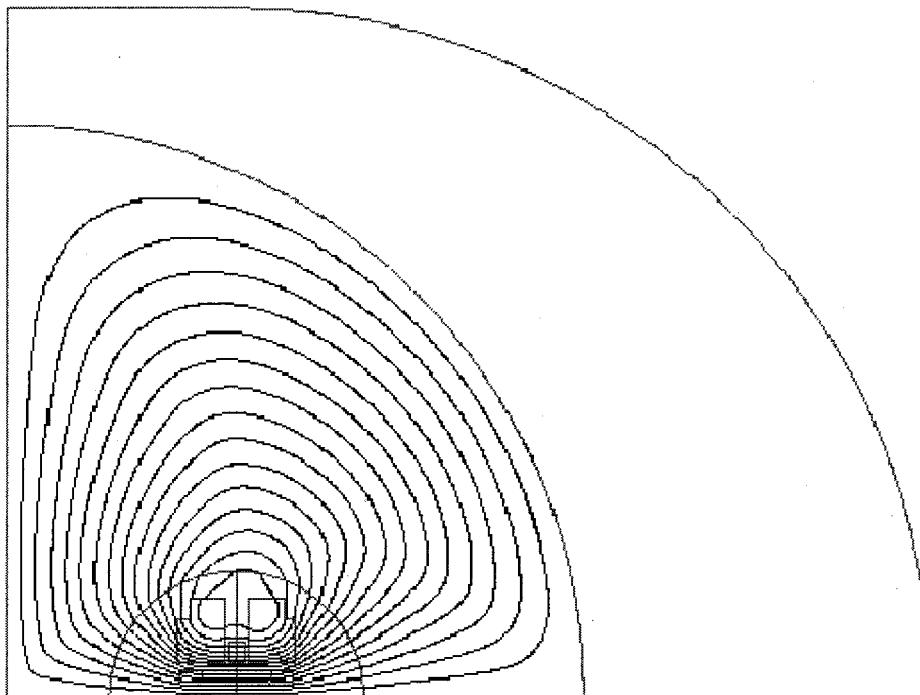
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Vertical two-in-one layout



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Vertical two-in-one layout

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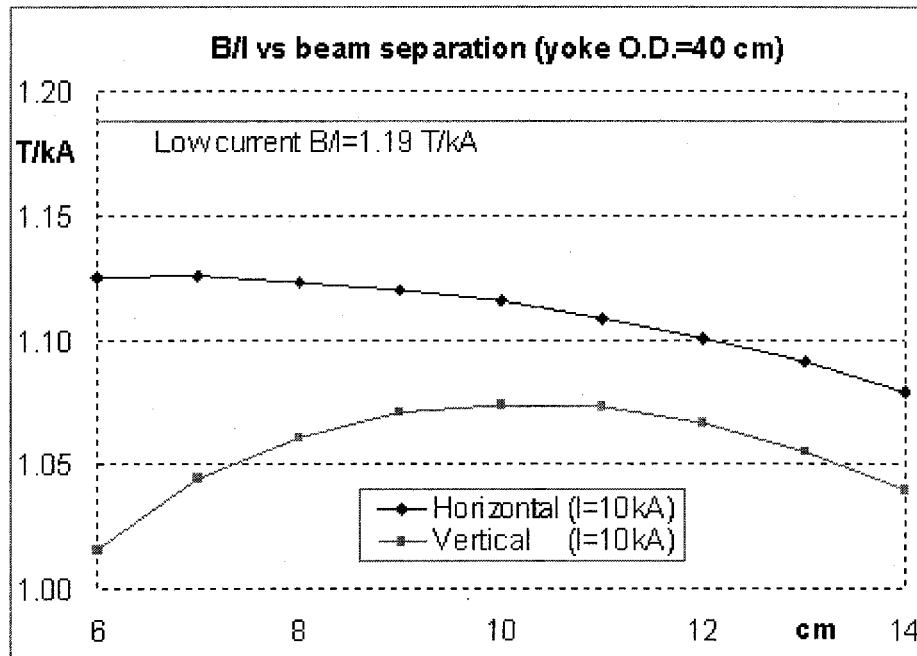
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Transfer function for 40 cm yoke diameter



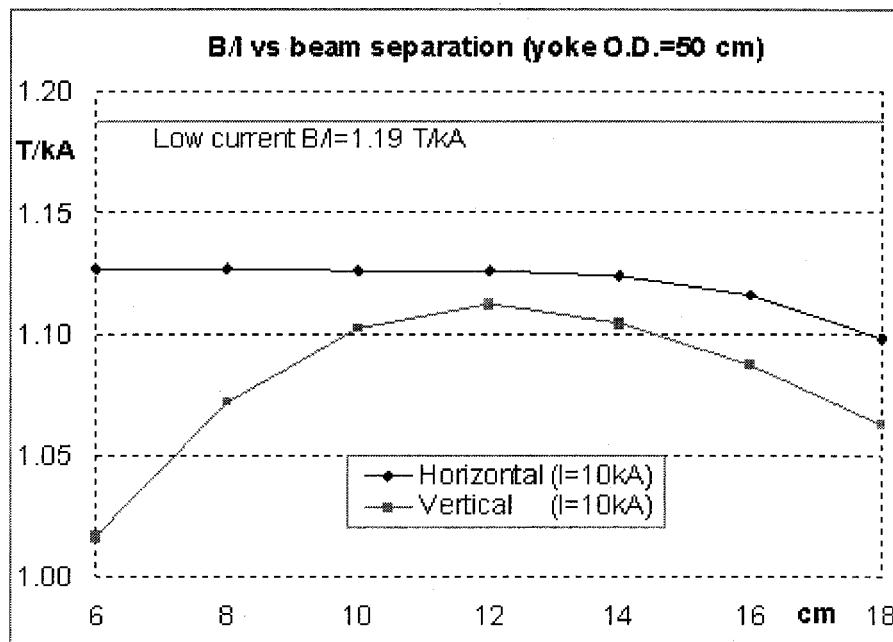
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Transfer function for 50 cm yoke diameter



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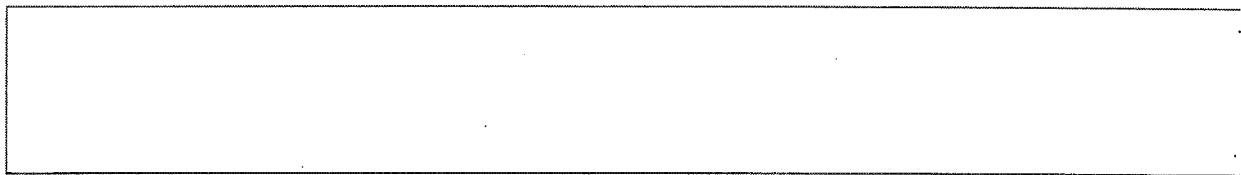
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Next steps

- Field quality: further optimize geometric harmonics, evaluate magnetic measurement accuracy.
- End field quality (in particular for block type designs).
- Mechanical parameters for conductor groups in the end regions (for shell type design).

Conclusions

- 30 mm bore dipole with 12-13 T design field using Nb₃Sn conductor at 4.2 K allows substantial savings in superconductor wrt 50 mm bore mag with same design parameters.
- For these design parameters, shell and block designs are substantially equivalent in terms of conduct efficiency and field quality.
- Vertical arrangement of the two apertures requires 50% larger yoke radius wrt horizontal arrangement in order to achieve same transfer function.



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